Composite Materials for Low Mass Stable Structures

LBNL Composites Shop, Mechanical Engineering Department, Engineering Division

Detector Supports for HEP Experiments

Tracking Detectors require support structures with low mass to reduce Coulomb Scattering of particle tracks thru the structure layers. Scattering and Stability detract from detector resolution equally. High Specific Stiffness materials E/X_0 are ideal for detector supports.

Global Supports and Integrating structures for Detectors are a core competency. These are typically thin-wall (0.6-0.8mm) cylinders, up to 8m assembled length. Eccentric stiffeners and mounts with composite bolted flanges are typical. Bonded Assembly procedures and tooling allow for precision of $+/-50\mu m$

Supported Detectors are often 10X the mass of the support structure Structures shown at left are used to both support and install multiple layers of Silicon Detectors around Be Beam pipes and are installed at the hearts of HEP/RNC colliding detectors





BNL Composite Shop was established to provide structures for the ATLAS Pixel System in 2002. Since then we have provided structures to both upgrade projects at RHIC and continued R&D efforts for sLHC upgrade

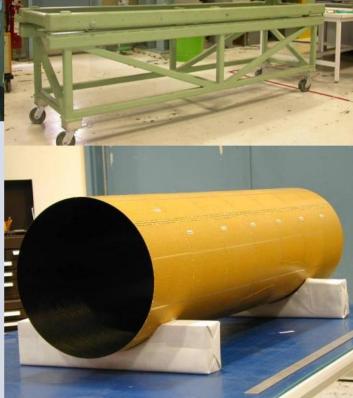
Process Equipment



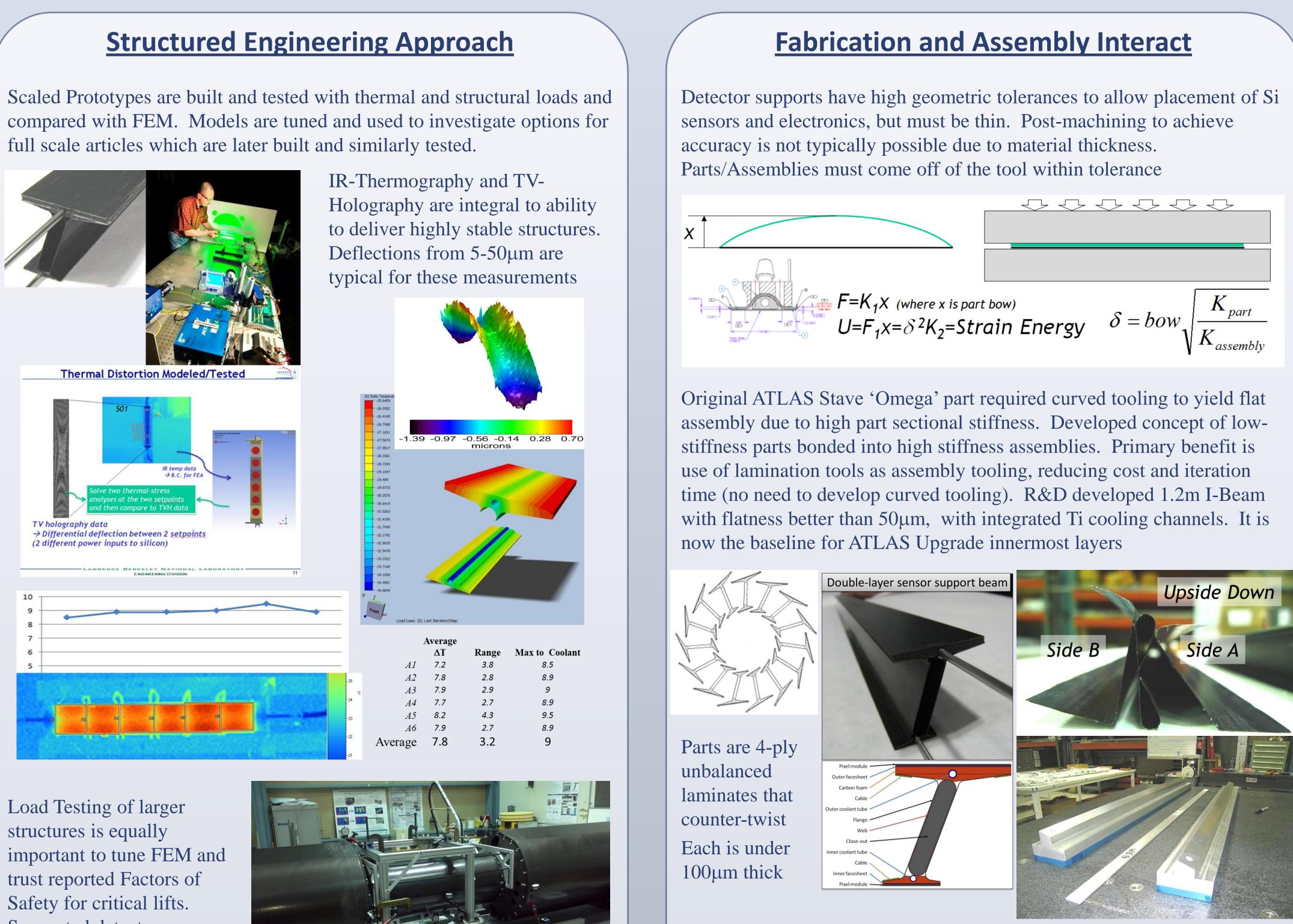
5X10 ASC Autoclave is fully automated, with integrated QC Database. Can process parts up to 1.2m X 2.7m, 150C cure temps with current pressurization system



www.PosterPresentations.com

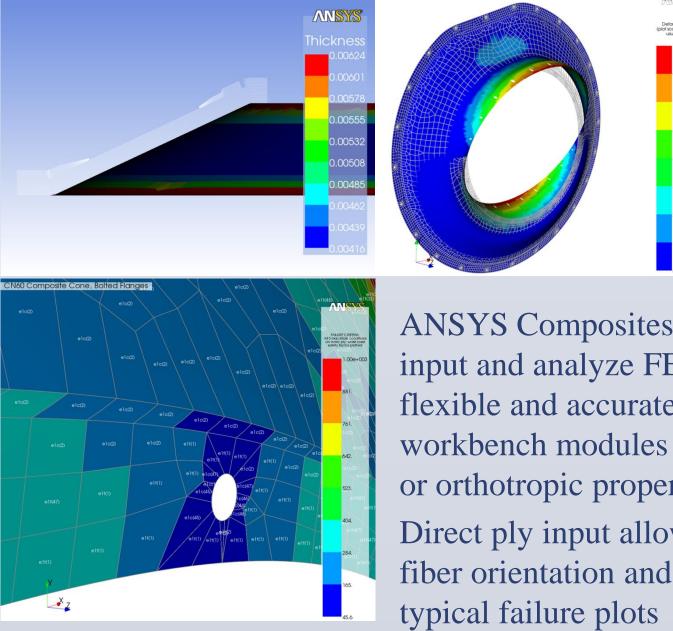


Automated Ply Cutter is used to minimize out-time of frozen Prepreg materials. Material/Part tracking DB links serial parts to production batches, tracks outlife and assures material remains in-spec—developed in-house by CAD Support Group

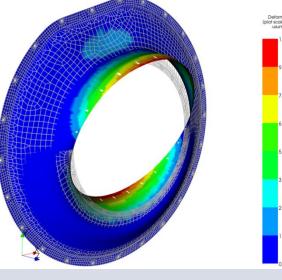


Supported detectors are often multi-million dollar deliverables





Analysis Tools



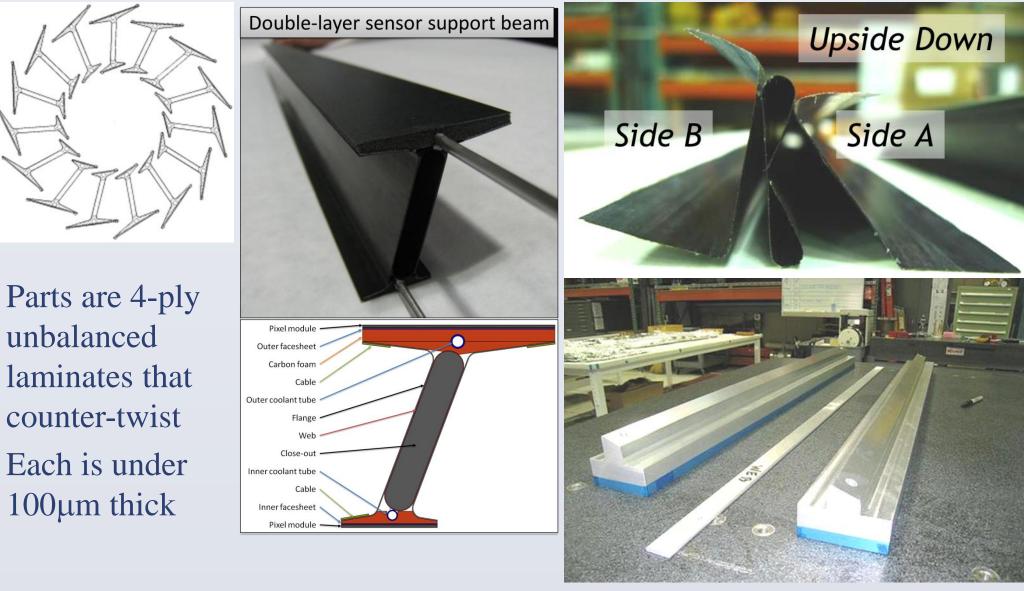
Cone Analysis showing Ply stack, Deformation and Fiber Failure plots

ANSYS Composites Pre/Post (ACP) used to input and analyze FEM results. Much more flexible and accurate than legacy or workbench modules which allow only ABD or orthotropic property inputs. Direct ply input allows tighter control of fiber orientation and standard outputs of

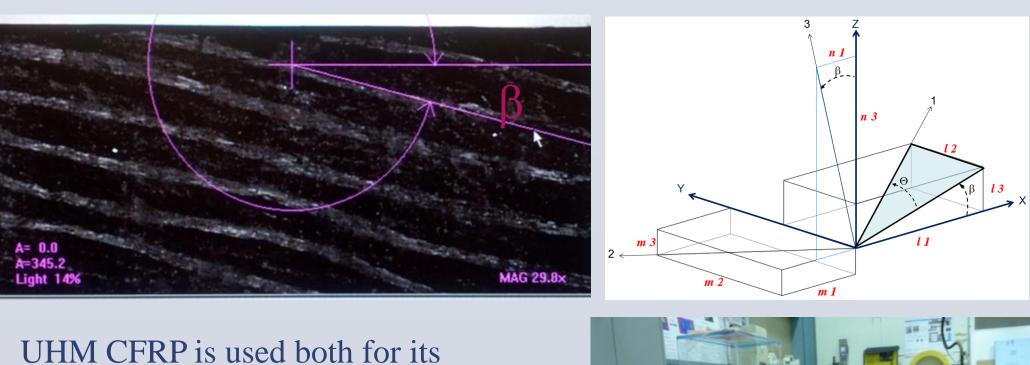
Micromechanics, lamina properties, and correlation with sample tensile/bend tests use MATLAB/Mathcad

iber and Matrix Properties (Input Values) Modulus CTE Poisson Ratio Fiber and Matrix Shear Moduli (Calculated Values) $\underline{G}_{\underline{12f}} := \frac{\underline{E}_{\underline{1f}}}{2 \cdot (1 - \underline{\nu}_{\underline{12f}})}$ $\underline{\mathbf{G}}_{\underline{23f}} := \frac{\underline{\mathbf{E}}_{\underline{2f}}}{2 \cdot (1 - \underline{\nu}_{\underline{12f}})}$ $\underline{G}_{\underline{m}} := \frac{\underline{E}_{\underline{m}}}{2 \cdot (1 - \underline{\nu}_{\underline{m}})}$

amina Properties <u>Cloth_Compliance</u> := 13% Modulus Fiber (1) Direction Modulus Orthogonal 2/3 Direction $E_{\underline{1}\underline{1}} := \frac{(\underline{E}_{\underline{1}\underline{f}}, \underline{V}_{\underline{f}} + \underline{E}_{\underline{m}}, \underline{V}_{\underline{j}})}{1 + \underline{Cloth}_{\underline{c}} Compliance} \qquad E_{\underline{2}\underline{2}} := \frac{\underline{E}_{\underline{m}}}{1 - \underline{V}_{\underline{f}} \left(1 - \frac{\underline{E}_{\underline{m}}}{\underline{E}_{\mathcal{F}}}\right)}$ $\underline{G_{\underline{12}}} \approx \frac{\underline{G_{\underline{m}}}}{1 - \underline{Y}_{\underline{f}} \cdot \left(1 - \frac{\underline{G}_{\underline{m}}}{\underline{G}_{\underline{12f}}}\right)} \qquad \underline{G}_{\underline{23}} \approx \frac{\underline{G}_{\underline{m}}}{1 - \underline{Y}_{\underline{f}} \cdot \left(1 - \frac{\underline{G}_{\underline{m}}}{\underline{G}_{\underline{22f}}}\right)} \qquad \underline{G}_{\underline{13}} \approx \underline{G}_{\underline{12}}$ $\underline{\nu_{12}} \coloneqq \underline{\nu_{12}} f \underline{V}_{1} + \underline{\nu_{11}} \underline{V}_{1} \qquad \underline{\nu_{22}} \coloneqq \frac{\underline{E_{22}}}{2\underline{G_{22}}} - 1 \qquad \underline{\nu_{13}} \coloneqq \underline{\nu_{12}} \qquad \underline{\nu_{21}} \coloneqq \underline{\nu_{12}} \frac{\underline{E_{22}}}{\underline{E_{11}}}$



Composite material properties are only beginning to be standardized for industrial use. The push is for intermediate modulus materials for strength driven designs (airframe structures). We typically use Ultra High Modulus fibers common to satellite structures. Functionally every order is a custom material, and fabrication methods can yield unique properties.

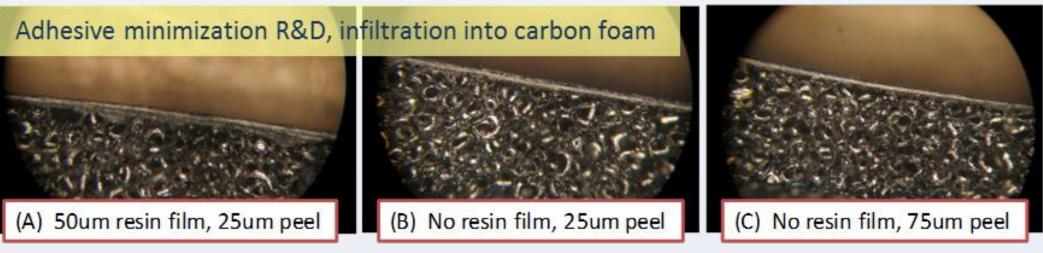


stiffness, but also it's thermal conductivity. Thru thickness conductivity is desirable for some thermal applications. Use of CFRP versus C-C (Carbon-Carbon) has potential cost benefits and schedule flexibility. Currently prototyping inclined plane laminates, and developing micromechanics via testing.

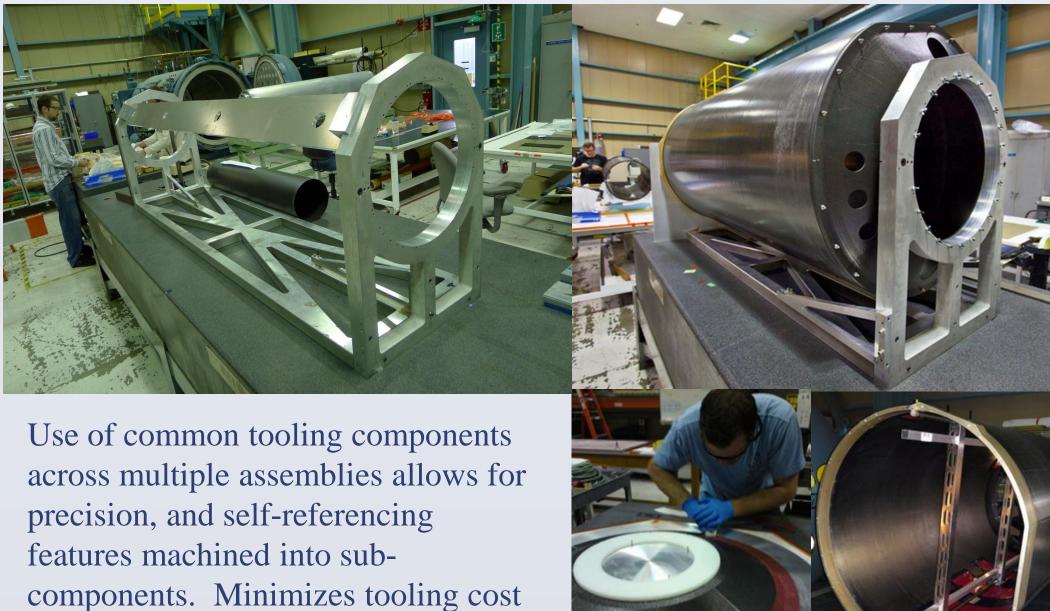
Material Development

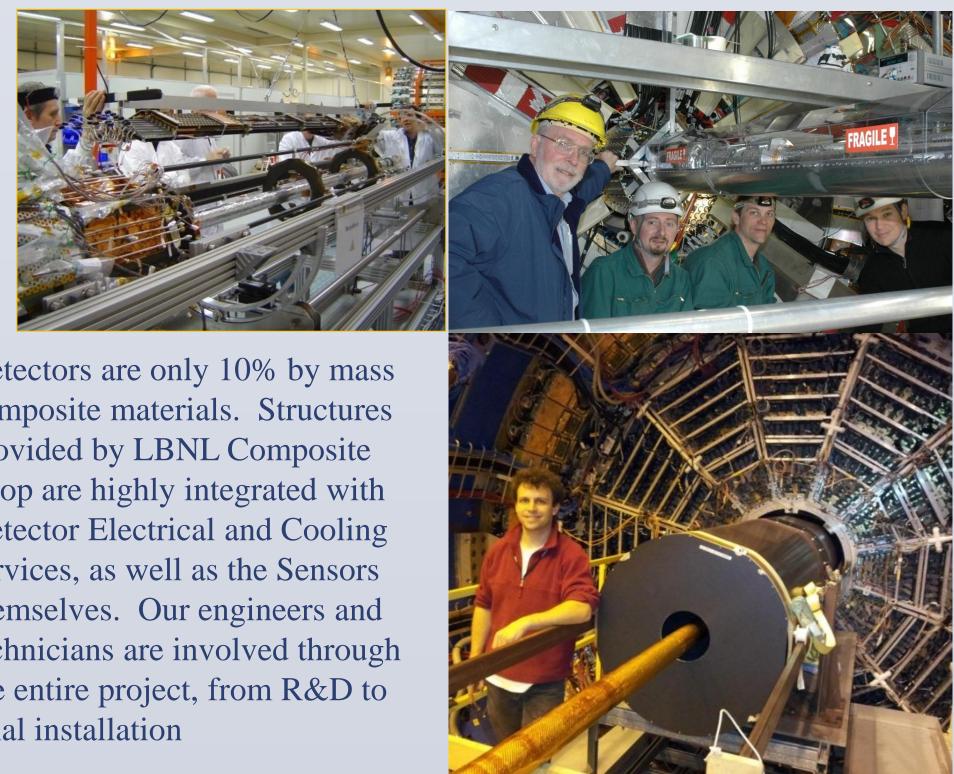


With laminates approaching the thickness of a typical bonded joint, adhesive mass is important to control for low mass structures. Resin content of custom prepregs can be tailored to allow co-cured components with no additional adhesive. For some of these low mass structures, adhesive can be 30-50% of the overall mass if not well controlled.



A combination of in-house and nearby machining capability is used to deliver and modify tooling for lamination and assembly tooling





Detectors are only 10% by mass composite materials. Structures provided by LBNL Composite Shop are highly integrated with Detector Electrical and Cooling services, as well as the Sensors themselves. Our engineers and technicians are involved through the entire project, from R&D to final installation



Process Optimization

Tooling Design and Fabrication

while maintaining required precision



Integration and Assembly